

Product evaluation and reaction modelling for the devolatilization of large coal particles



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Thesis submitted in fulfilment of the requirements for the degree

Philosophiae Doctor in Chemical Engineering

in the School of Chemical and Minerals Engineering at the Potchefstroom campus of the
North-West University, South Africa.

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November 2012

“Science can only ascertain what is, but not what should be, and outside of its domain value judgements of all kinds remain necessary.”

- Albert Einstein-

Declaration

I, Barend Burgert Hattingh, hereby declare that the thesis entitled: "***Product evaluation and reaction modelling for the devolatilization of large coal particles***", submitted in fulfilment of the requirements for the degree Ph.D in chemical engineering is my own work, except where acknowledged in the text, and has not been submitted to any other tertiary institution in whole or in part.

Signed at Potchefstroom

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Date

Acknowledgements

The success of this investigation has been mainly dependent on the involvement of a few important people/parties. The author hereby wishes to acknowledge and thank all the people/parties involved during the course of this project and would like to send out a special wish of gratitude to the following:

- Our heavenly Father for blessing and providing me with the opportunity to study. Furthermore for the guidance, courage and determination that was given to me through the course of this investigation and my entire life;
- My study coordinators Professors Ray Everson, Hein Neomagus, John Bunt and Dr. Daniel van Niekerk for their excellent guidance, assistance and willingness to help. Without their critical evaluation of this thesis and the priceless suggestions this investigation would not have been a success;
- Sasol for their financial support with respect to this investigation;
- Anglo coal and Exxaro for supplying the respective coals;
- Mr. Johan de Korte (CSIR) for his involvement in the arrangement of the coal samples;
- Mr. David Powell (Exxaro) for arranging and conducting the preliminary preparation (screening) of the TSH coal samples;
- Prof. Hein Neomagus for his friendship and the fruitful discussions regarding the design and development of the tar capturing apparatus;
- Mr. Jan Kroeze, Mr. Adrian Brock, Mr. Ted Paarlberg and Mr. Johan Broodryk for the construction of the tar capturing apparatus and the additional accessories for successfully capturing coal tars during devolatilization;
- Another word of appreciation to Dr. Daniel van Niekerk who assisted in the training, interpretation and analyses (SIMDIST, GC-MS, GC-FID and SEC) of the coal-derived tars;
- Sasol Infrachem® for performing SIMDIST, GC-MS and GC-FID on the generated tar samples.
- Dr. Alan Herod (Imperial College) for his thoughts and suggestions regarding tar production and -tar capturing strategies;
- Dr. Jonathan Mathews (Pennsylvania State University) for his valuable comments regarding advanced analyses on coals and chars as well as for his involvement in MALDI-TOF analyses of the four coals;

- Mr. Ben Ashton for his assistance with non-isothermal TGA measurements at Sasol;
- Prof. Nicola Wagner (University of Witwatersrand) for the morphological analyses conducted on the produced chars;
- Mr. Mokone Roberts for his assistance and valuable inputs during the development of the HRTEM image processing technique;
- Mr. Gregory Okolo for his involvement in establishing the XRD carbon crystallite method at the NWU;
- Dr. Johan Jordaan and Mr. Andre Joubert for their assistance and suggestions in developing analytical competency at the North West University in coal tar analyses via GC-MS and NMR;
- Dr. Jaco Brand from Stellenbosch University for assisting in the ^1H - and ^{13}C NMR analyses on the tar samples;
- Mr. Arno Hattingh (4th year student) for his assistance in evaluating the temperature profiles of the large coal particles;
- The coal group for their good nature and lively spirit during the past five years of my involvement with this astounding research entity;
- Mr. Francois Stander and Mr. Elmar Prinsloo for their friendship, assistance and suggestions during the course of my experimentation;
- My parents and my sister for their moral support, guidance and love;
- Last but definitely not the least, Monique Loock, my fiancée; for her love, moral support and assistance in dark times. Without you, hope would have been lost long before completion of this thesis!!!

Title page and chapter pictures:

Anon. 2012. Chemical plant-High resolution.

<http://www.onlyhdwallpapers.com/flower/chemical-plant-high-resolution-desktop-HD-wallpaper-340464.jpg> Date of access: 30 September 2012.

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Abstract

A fundamental understanding of the process of devolatilization requires extensive knowledge of not only the intrinsic properties of the parent coal and its subsequent formed products (tars, gases and chars), but also its characteristic reaction rate behaviour. Devolatilization behaviour has been extensively addressed in literature with the use of powdered coal samples, which normally do not adhere to particle size constraints of coal conversion processes utilizing lump coal. The aim of this investigation was therefore to assess the devolatilization behaviour (with respect to product yield and -quality; and reaction rate modelling) of four typical South African coals (UMZ, INY, G#5 and TSH) confined to the large particle regime. All four coals were found to be bituminous in rank, with vitrinite contents ranging between 24.4 vol.% and 69.2 vol.% (mineral matter free basis). Two were inertinite-rich coals (UMZ and INY) and the other two were vitrinite-rich coals (G#5 and TSH). From thermoplasticity measurements it was evident that only coal TSH displayed extensive thermoplastic behaviour, while a comparison between molecular properties confirmed the higher abundance of poly-condensed aromatic structures (aromaticity of 81%) present in this coal.

Product evolution was evaluated under atmospheric conditions in a self-constructed, large particle, fixed-bed reactor, on two particle sizes (5 mm and 20 mm) at two isothermal reactor temperatures (450 °C and 750 °C) using a combination of both GC and MS techniques for gas species measurement, while standard gravimetric methods were used to quantify tar- and char yield respectively. Elucidation of tar- and char structural features involved the use of both conventional- and advanced analytical techniques. From the results it could be concluded that temperature was the dominating factor controlling product yield- and quality, with significant increases in both volatile- and gas yield observed for an increase in temperature. Tar yields ranged between 3.6 wt.% and 10.1 wt.% and increased in the order UMZ < INY < TSH < G#5, with higher tar yields obtained for coal G#5, being ascribed to larger abundances of vitrinite and liptinite present in this coal. For coal TSH, lower tar yields could mainly be attributed to the higher aromaticity and extensive swelling nature of this coal. Evolved gases were found to be mainly composed of H₂, CH₄, CO and CO₂, low molecular weight olefins and paraffins; and some C₄ homologues. Advanced analytical techniques (NMR, SEC, GC-MS, XRD, etc.) revealed the progressive increase of the aromatic nature of both tars and chars with increasing temperature; as well as subsequent differences in tar composition between the different parent

coals. In all cases, an increase in devolatilization temperature led to the evolution of larger amounts of aromatic compounds such as alkyl-naphthalenes and PAHs, while significant decreases in the amount of aliphatics and mixed compounds could be observed. From ^{13}C NMR, HRTEM and XRD carbon crystallite results it was clear that an increase in temperature led to the formation of progressively larger, more aromatic and structurally orientated poly-condensed carbon structures.

Reaction rate studies involved the use of non-isothermal (5-40 K/min) and isothermal (350-900°C) thermogravimetry of both powdered ($-200\ \mu\text{m}$) and large particle samples (20 mm) in order to assess intrinsic kinetics and large particle rate behaviour, respectively. Evaluation of the intrinsic kinetic parameters of each coal involved the numerical regression of non-isothermal rate data in MATLAB[®] 7.1.1 according to a pseudo-component modelling philosophy. Modelling results indicated that the intrinsic devolatilization behaviour of each coal could be adequately described by using a total number of eight pseudo-components, while reported activation energies were found to range between 22.3 kJ/mol and 244.3 kJ/mol. Description of the rate of large particle devolatilization involved the evaluation of a novel, comprehensive rate model accounting for derived kinetics, heat and mass transport effects, as well as physical changes due to particle swelling/shrinkage. Evaluation of the proposed model with the aid of the COMSOL Multiphysics 4.3 simulation software provided a suitable fit to the experimental data of all four coals, while simulation studies highlighted the relevant importance of not only the effect of particle size, but also the importance of including terms affecting for heat losses due to particle swelling/shrinkage, transport of volatile products through the porous char structure, heat of reaction and heat of vaporization of water.

Keywords: South African coal, devolatilization, large particles, tar, char, reaction modelling.

Opsomming

'n Fundamentele begrip van die proses van termiese ontgassing (pirolise) vereis ekstensiewe kennis van nie net die intrinsieke eienskappe van die oorspronklike steenkool en sy daaropvolgende produkte (tere, gasse en sintels) nie, maar ook die karakteristieke tempo waarteen die betrokke steenkool reageer. Alhoewel pirolisegedrag van verpoeierde steenkoolmonsters reeds breedvoerig aangespreek is in beskikbare literatuur, is wynig egter bekend oor die pirolisegedrag van groot partikels, kenmerkend van groot-partikel steenkoolomsettingsprosesse. Die doel van hierdie ondersoek was dus om die pirolise gedrag (m.b.t. produkopbrengs en –gehalte, asook reaksie modellering) van vier tipies, Suid-Afrikaanse steenkole (UMZ, INY, G#5 en TSH), beperk tot groot partikel monsters, te assesseer. Al vier steenkole is geklassifiseer as bitumineuse rang steenkole met vitriniet inhoude tussen 24.4 vol.% en 69.2 vol.% (mineraal-vry basis). Twee hiervan was inertiniet-ryke steenkole (UMZ en INY) en die ander twee was vitriniet-ryke steenkole (G#5 en TSH). Vanuit termoplastiese analyses is dit bevind dat slegs steenkool TSH drastiese termoplastiese gedrag vertoon, terwyl 'n vergelyking tussen molekulêre eienskappe bevestig het dat hierdie steenkool ook gekenmerk word aan 'n hoër konsentrasie van poli-gekondenseerde aromatisiese strukture (aromatisiteit van 81%). Produktvorming is bestudeer onder atmosferiese kondisies in 'n self-vervaardigde, groot-partikel, vaste-bed reaktor deur gebruik te maak van twee partikel groottes (5 mm en 20 mm) en twee isotermiese reaksie temperature (450°C en 750°C). Gasspesieontwikkeling is gemonitor deur gebruik te maak van 'n kombinasie van beide gaschromatografie (GC) en massaspektrometrie (MS) tegnieke, terwyl standaard gravimetriese metodes gebruik is om teer en sintel opbrengs onderskeidelik te kwantifiseer. Hiermee saam, is die gebruik van konvensionele- en gevorderde analitiese metodes ingespan om die strukturele eienskappe van beide die gevormde tere en sintels te evalueer. Vanuit die resultate was dit dus duidelik dat temperatuur die oorheersende faktor is wat die opbrengs en kwaliteit van die gevormde produkte beïnvloed. Gevolglik is 'n beduidende toename in beide vlugtige produk- en gasopbrengs waargeneem vir 'n toename in reaksietemperatuur, terwyl teeropbrengste gewissel het tussen 3.6 gewigs % en 10.1 gewigs %. Verder is dit bevind dat teeropbrengste verhoog het in die volgorde UMZ < INY < TSH < G#5, met die hoër opbrengs van steenkool G#5 toeskryfbaar aan die groter hoeveelhede vitriniet en liptiniet teenwoordig in hierdie steenkool. Die laer teer opbrengs verkry vir steenkool TSH kon egter toegeskryf word aan beide die hoër aromatisiteit en uitermatige swel eienskappe van hierdie steenkool. Vrygestelde gasse

het hoofsaaklik bestaan uit H_2 , CH_4 , CO en CO_2 , lae molekulêre gewig olefiene en parafiene; asook 'n paar C_4 homoloë. Gevorderde analitiese tegnieke soos kern magnetiese resonansspektroskopie (KMR), grootte-uitsluitings chromatografie (SEC), X-straal diffraksie (XRD), gaschromatografie-massaspektrometrie (GC-MS) ens. het nie net bewys gelewer van die progressiewe verhoging in die aromatiese karakter van beide die tere en sintels met 'n toename in temperatuur nie, maar het ook daaropvolgende verskille in teer samestelling tussen die verskillende steenkole uitgelig. 'n Toename in pirolisetemperatuur is dus gekenmerk deur die produksie van groter hoeveelhede aromatiese verbindings soos alkiel-naftalene en polisikliese aromatiese koolwaterstowwe (PAKs), terwyl aansienlike afnames in beide die hoeveelheid alifatiese- en vermengde verbindings egter waargeneem is. Vanuit ^{13}C KMR, HRTEM (hoë-resolusie transmissie-elektronmikroskopie) en XRD koolstof-kristallietanalises was dit verder duidelik dat 'n verhoging in temperatuur gelei het tot die vorming van groter en meer struktureel-georiënteerde, poli-gekondenseerde, aromatiese koolstofstrukture.

Pirolisereaktiwiteit is ondersoek op beide verpoeierde ($-200 \mu m$) en groot-partikel (20 mm) steenkoolmonsters deur onderskeidelik gebruik te maak van nie-isotermiese (5-40 K/min) en isotermiese (350-900 °C) termogravimetrie (TG) metodes, ten einde beide intrinsieke kinetika en groot-partikel reaksiegedrag te bestudeer. Intrinsieke kinetiese parameters van elke steenkool is numeries bepaal vanuit die nie-isotermiese TG resultate deur gebruik te maak van 'n pseudo-komponent modellerings filosofie in MATLAB[®] 7.1.1. Modelleringsresultate het gevolglik daarop gedui dat die intrinsieke pirolise gedrag van elke steenkool voldoende beskryf kon word deur 'n totaal van agt pseudo-komponent reaksies waarvan aktiveringsenergieë wissel tussen 22.3 kJ/mol en 244.3 kJ/mol. Na aanleiding hiervan kon pirolise gedrag van die groot steenkoolpartikels dus beskryf word deur 'n omvattende model wat rekening hou met reaksiekinetika, hitte- en massaordrageffekte, asook fisiese veranderinge weens partikel swelling/krimping. Modelling met behulp van die COMSOL Multiphysics[®] 4.3 simulatiepakket het daarop gedui dat die eksperimentele resultate bevredigend beskryf kon word deur die voorgestelde groot-partikel model, terwyl simulatie studies die belangrikheid van die effek van partikelgrootte en die effek van die insluiting van hitteverlies weens partikel termoplastisiteit, massaordrag van vlugtige produkte deur die poreuse sintelstruktuur, reaksie-entalpie en die verdamping van water beklemtoon het.

Kernwoorde: Suid-Afrikaanse steenkool, pirolise, groot partikels, teer, sintels, reaksie modellering.

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List of Symbols

ROMAN SYMBOLS

Symbol	Description	Units
a	<i>Kinetic compensation constant</i>	-
b	<i>Kinetic compensation constant</i>	K^{-1}
$B.L.$	<i>Number of bridges and loops</i>	-
C	<i>Number of aromatic carbons per cluster</i>	-
C_A	<i>Acenaphthene type aliphatic carbons</i>	%
C_{Al}	<i>Aliphatic carbons</i>	%
C_{Ar}	<i>Aromatic carbons</i>	%
C_{Ar1}	<i>Aromatic carbons (C_{ar-H} ortho to C_{ar-OH})</i>	%
C_{Ar2}	<i>Aromatic carbons (C_{ar-H} para to C_{ar-OH}, etc.)</i>	%
C_{Ar3}	<i>Aromatic carbons (C_{ar-CH_3} para to C_{ar-OH})</i>	%
C_{Ar4}	<i>Quaternary aromatic carbons; C_{ar-H} meta to C_{ar-OH}</i>	%
C_{Ar5}	<i>Aromatic carbons (C_{ar-CH_3}; CH_2 or CH para to C_{ar-OH})</i>	%
C_{Ar6}	<i>Aromatic carbons (CH_2 or CH meta to C_{ar-OH})</i>	%
C_{Ar7}	<i>Aromatic carbons (C_{ar-OH})</i>	%
C_{ArP}	<i>Pericondensed aromatic- or protonated aromatic carbons</i>	%
C_{ArC}	<i>Catacondensed aromatic carbons</i>	%
C_{ave}	<i>Average number of carbon atoms</i>	-
C_F	<i>Fluorene type aliphatic carbons</i>	%
CH_2	<i>Methylene (CH_2) and methine (CH) carbons α</i>	%
CH_3	<i>Methyl carbons</i>	%
C_{max}	<i>Maximum number of carbon atoms</i>	-
C_{min}	<i>Minimum number of carbon atoms</i>	-
$C_{\alpha 2}$	<i>Methylene and methine carbons α to two aromatic rings</i>	%
$c_{p,a}$	<i>Mass specific heat capacity for water</i>	$J.kg^{-1}.K^{-1}$
$c_{p,s}$	<i>Mass specific heat capacity for coal</i>	$J.kg^{-1}.K^{-1}$
$c_{p,v}$	<i>Mass specific heat capacity for volatiles</i>	$J.kg^{-1}.K^{-1}$
d_{002}	<i>Interlayer spacing</i>	Å

ROMAN SYMBOLS (CONTINUED)

Symbol	Description	Units
d_p	<i>Diameter of coal particle</i>	m
d_{pore}	<i>Pore diameter</i>	Å
D_{a-air}	<i>Binary diffusion coefficient for water vapour and air</i>	$m^2 \cdot s^{-1}$
D_{ik}	<i>Knudsen diffusion of species i (a or v)</i>	$m^2 \cdot s^{-1}$
D_{eff}	<i>Effective diffusion coefficient</i>	$m^2 \cdot s^{-1}$
$D'_{eff,i}$	<i>Effective diffusion coefficient of i (a or v)</i>	$m^2 \cdot s^{-1}$
$D_{eff,i}$	<i>Effective diffusion coefficient of species i (a or v)</i>	$m^2 \cdot s^{-1}$
D_{v-air}	<i>Binary diffusion coefficient for volatiles and air</i>	$m^2 \cdot s^{-1}$
D_{t-gv}	<i>Binary diffusion coefficient for tar and volatile gas</i>	$m^2 \cdot s^{-1}$
DOI	<i>Degree of disorder index</i>	-
E_0	<i>Mean activation energy for DAEM</i>	$kJ \cdot mol^{-1}$
E_a	<i>Activation energy</i>	$kJ \cdot mol^{-1}$
$E_{a,a}$	<i>Activation energy of moisture evolution</i>	$kJ \cdot mol^{-1}$
$E_{a,i}$	<i>Activation energy of component i</i>	$kJ \cdot mol^{-1}$
E_l	<i>Exponential integral</i>	-
f_a	<i>Aromaticity/Fraction of aromatic carbon</i>	-
f_a'	<i>Corrected fraction of aromatics (excluding CO)</i>	-
f_a^B	<i>Fraction of bridgehead carbons</i>	-
f_a^{CO}	<i>Fraction of carbonyl/carboxyl functionalities</i>	-
f_a^H	<i>Fraction of protonated aromatic carbons</i>	-
f_a^N	<i>Fraction of non-protonated aromatic carbons</i>	-
f_a^P	<i>Fraction of phenolic functionalities</i>	-
f_a^S	<i>Fraction of alkylated aromatic carbons</i>	-
f_{al}	<i>Fraction of aliphatic carbons</i>	-
f_{al}^*	<i>Fraction of non-protonated aliphatic carbons</i>	-
f_{al}^H	<i>Fraction of protonated aliphatic carbons</i>	-
f_{al}^O	<i>Fraction of oxygenated aliphatic carbons</i>	-
FC	<i>Fixed carbon</i>	wt. %
$F_{VM,i}$	<i>Amount of component i, w.r.t. ultimate volatile yield</i>	wt. %
h_{conv}	<i>External/convective heat transfer coefficient</i>	$W \cdot m^{-2} \cdot K^{-1}$
H_{Al}	<i>Aliphatic protons</i>	%

ROMAN SYMBOLS (CONTINUED)

Symbol	Description	Dimension
H_{Ar}	Aromatic protons	%
H_{ArUC}	Aromatic hydrogen	%
H_{ArC}	Sterically hindered aromatic hydrogen	%
$H_{A,F}$	Acenaphthene and fluorine type protons	%
H_D	Diphenylmethane type protons	%
H_O	Olefinic protons	%
$H_{\alpha 1}$	Aliphatic protons methyl or methylene in α position	%
$H_{\beta 1}$	Aliphatic protons methyl or methylene in β position	%
$H_{\beta 2}$	Alicyclic protons methyl or methylene in γ position	%
H_{γ}	Aliphatic protons to two aromatics in β position	%
ΔH_r	Enthalpy/heat of reaction	kJ.kg^{-1}
$\Delta H_{vap,a}$	Enthalpy/heat of evaporation of water	J.kg^{-1}
HV	Heating value / Gross Calorific Value	MJ/kg
HVF	Heating Value Factor	-
$I_{main\ peak}$	Fractional amount of main peak associated to inertinite	-
INR	Non-reactive inertinite macerals (mineral matter free basis)	vol.%
INT	Inertinite content (mineral matter free basis)	vol.%
k	Rate constant	s^{-1} or min^{-1}
K	Constant depending on X-ray reflection plane	-
$K_{\alpha 1}$	X-ray radiation from cobalt due to $K_{\alpha 1}$	counts
$K_{\alpha 2}$	X-ray radiation from cobalt due to $K_{\alpha 2}$	counts
k_0	Pre-exponential constant	s^{-1} or min^{-1}
$k_{0,a}$	Pre-exponential constant of moisture evolution	s^{-1}
$k_{0,i}$	Pre-exponential constant of the i^{th} pseudo-component	s^{-1}
k_g	Heat/thermal conductivity of heating medium (N_2)	$\text{W.m}^{-1}.\text{K}^{-1}$
K_p	Permeability of coal	m^2
k_s	Solid effective heat/thermal conductivity	$\text{W.m}^{-1}.\text{K}^{-1}$
L_a	Crystallite diameter	Å
L_c	Crystallite height	Å
$L_{main\ peak}$	Fractional amount of main peak associated to liptinite	-
LIP	Liptinite content (mineral matter free basis)	vol.%

ROMAN SYMBOLS (CONTINUED)

Symbol	Description	Dimension
m_0	<i>Initial sample mass</i>	mg
m_{ash}	<i>Ash mass</i>	mg
$m_{ash,raw}$	<i>Original ash mass value</i>	mg
$m_{ash,demin}$	<i>Demineralised coal ash mass value</i>	mg
m_f	<i>Final sample mass</i>	mg
m_t	<i>Logged mass at a certain time t</i>	mg
M_a	<i>Molecular weight of water</i>	$\text{g}\cdot\text{mol}^{-1}$
M_{air}	<i>Molecular weight of air</i>	$\text{g}\cdot\text{mol}^{-1}$
$MaxL$	<i>Maximum fringe length</i>	Å
m_{coal}	<i>Mass of coal</i>	mg or g
M_G	<i>Fraction of aromatic carbons with attached proton</i>	-
MR_i	<i>Maximum weight loss rate of peak i, in DTG curve</i>	min^{-1}
$MinL$	<i>Minimum fringe length</i>	Å
M_{gv}	<i>Molecular weight of devolatilization gas</i>	$\text{g}\cdot\text{mol}^{-1}$
MI	<i>Maceral index</i>	-
M_n	<i>Number average molecular weight</i>	$\text{g}\cdot\text{mol}^{-1}$ or Da
m_p	<i>Mass of particle</i>	mg
M_p	<i>Molecular weight estimate from SEC</i>	$\text{g}\cdot\text{mol}^{-1}$ or Da
m_{pl}	<i>Mass of submerged plunger</i>	mg
m_{sb}	<i>Mass of submerged particle</i>	mg
M_t	<i>Molecular weight of tars</i>	$\text{g}\cdot\text{mol}^{-1}$
M_v	<i>Average molecular weight of volatiles</i>	$\text{g}\cdot\text{mol}^{-1}$
$M_{r,i}$	<i>Molecular weight of species, i</i>	$\text{g}\cdot\text{mol}^{-1}$
$M_{w,p}$	<i>Weight average molecular weight</i>	$\text{g}\cdot\text{mol}^{-1}$
M_w	<i>Molecular weight of fringe</i>	$\text{g}\cdot\text{mol}^{-1}$
MW	<i>Average molecular weight of cluster</i>	$\text{g}\cdot\text{mol}^{-1}$
M_5	<i>Average molecular weight of side chain or half of bridge</i>	$\text{g}\cdot\text{mol}^{-1}$
n	<i>Reaction order</i>	-
\dot{n}_i	<i>Mass flux of species, i</i>	$\text{kg}\cdot\text{m}^{-3}\cdot\text{s}^{-1}$
N_{ave}	<i>Average number of layers per carbon crystallite</i>	-
N_k	<i>Number of heating rates</i>	-

ROMAN SYMBOLS (CONTINUED)

Symbol	Description	Dimension
N_m	Number of DTG experimental points	
n_T	Total molar flow of N_2 gas	mol.min ⁻¹
OBF	Objective function	-
p	Pressure	Pa
p_0	Initial ambient pressure	Pa
P_0	Number of all possible bridges intact	-
p_i	Partial pressure of species i (a or v)	Pa
$p_{v,t}$	Total pressure of gas product mixture	Pa
P_i	Peak i , in DTG curve	-
Pr	Prandtl number	-
QOF	Quality of fit	%
r	Radial coordinate of coal particle	m
R	Molar gas constant	J.K ⁻¹ .mol ⁻¹
R_a	Intrinsic rate of moisture evaporation	kg.m ⁻³ .s ⁻¹
R_i	Intrinsic rate of the evolution of species, i	kg.m ⁻³ .s ⁻¹
Re	Reynolds number	-
RF	Reactivity Factor	-
RMI	Reactive maceral index	-
R_p	Radius of coal particle	m
R_r	Mean random vitrinite reflectance	%
R_v	Intrinsic rate of volatile evolution	kg.m ⁻³ .s ⁻¹
S_{002}	Area under the d_{002} peak	Intensity. Å
S_A	Area under the amorphous peak	Intensity. Å
S_G	Area under the graphitic peak	Intensity. Å
S_γ	Area under the γ -band	Intensity. Å
S.C.	Number of side chains per cluster	-
t	Time	s or min
t_∞	Infinite time	s or min
t_E	Elution time during SEC analyses	min
T	Temperature	°C or K
T_f	External temperature	°C or K

ROMAN SYMBOLS (CONTINUED)

Symbol	Description	Dimension
T_s	Coal particle temperature	°C or K
$T_{p,i}$	Temperature of local maxima of peak i , in DTG curve	°C or K
T_0	Initial temperature	°C or K
$T_{10 \text{ wt.}\%}$	SIMDIST temperature at 10 wt.% mass recovery	°C or K
$T_{30 \text{ wt.}\%}$	SIMDIST temperature at 30 wt.% mass recovery	°C or K
$T_{50 \text{ wt.}\%}$	SIMDIST temperature at 50 wt.% mass recovery	°C or K
$T_{70 \text{ wt.}\%}$	SIMDIST temperature at 70 wt.% mass recovery	°C or K
$T_{90 \text{ wt.}\%}$	SIMDIST temperature at 90 wt.% mass recovery	°C or K
$Tm_{1,calc}$	Calculated temperature of maximum global reactivity	°C or K
$Tm_{1,exp}$	Experimental temperature of maximum global reactivity	°C or K
ΔTm_1 ($I_{main \text{ peak}}$)	Parametric term of temperature prediction	°C or K
ΔTm_1 ($L_{main \text{ peak}}$)	Parametric term of temperature prediction	°C or K
$\Delta Tm_1(R_r)$	Parametric term of temperature prediction	°C or K
$\Delta Tm_1(R_t)$	Parametric term of temperature prediction	°C or K
u	Darcy velocity field of gas mixture (volatiles, air and vapour)	$m \cdot s^{-1}$
v_0	Initial particle volume	m^3
v	Coal particle volume	m^3
v_g	Superficial gas velocity of heating medium (N_2)	$m \cdot s^{-1}$
VIT	Vitrinite content (mineral matter free basis)	vol.%
VM	Volatile matter	wt.%
VM_j	Volatile matter contribution of maceral, j	wt.%
VM_{TGA}	Ultimate volatile yield from TGA results	wt.%
V_a^*	Ultimate amount of moisture evolved	- or %
V_i	Volatile yield of pseudo-component, i at time t	- or %
V_i^*	Ultimate volatile yield of pseudo-component, i	- or %
V_t^*	Ultimate volatile yield	- or %
V_t	Volatile yield at time, t	- or %
$V_{t,T}$	Total product yield (moisture and volatiles) at time t and temperature T	- or %

ROMAN SYMBOLS (CONTINUED)

Symbol	Description	Dimension
$V_{t,T}^*$	<i>Ultimate product yield (moisture and volatiles) at time t and temperature T</i>	- or %
$V_{t,v}^*$	<i>Ultimate total volatile yield</i>	- or %
WABP	<i>Weight average boiling point</i>	°C or K
X	<i>Fractional conversion</i>	-
X_a	<i>Fractional conversion of moisture evolution</i>	-
X_A	<i>Fraction amorphous carbon</i>	-
X_b	<i>Fractional conversion of peak b</i>	-
$X_{f,v}^*$	<i>Scaling factor/Final isothermal total conversion</i>	-
X_g	<i>Fractional conversion of the molecular phase</i>	-
X_i	<i>Fractional conversion of the i^{th} pseudo-component</i>	-
X_t	<i>Overall fractional conversion of volatiles</i>	-
X_v	<i>Fractional conversion of volatiles</i>	-
$X_{v,t}$	<i>Fractional conversion of volatiles at time, t</i>	-
$X'_{v,t}$	<i>Re-scaled/normalised fractional conversion of volatiles at time, t</i>	-
Y_j	<i>Content of maceral, j in the coal</i>	vol.%
Y_m	<i>Content of residual macerals in the coal</i>	vol.%

GREEK SYMBOLS

Symbol	Description	Units
α	<i>Kinetic compensation constant</i>	mol.kJ ⁻¹
α_{il}	<i>Rank dependent fractional contribution of inertinite</i>	-
α_{iL}	<i>Rank dependent fractional contribution of liptinite</i>	-
α_{iV}	<i>Rank dependent fractional contribution of vitrinite</i>	-
β	<i>Heating rate</i>	°C.min ⁻¹ /K.min ⁻¹
β_{002}	<i>Full width at half maximum of the d_{002} peak</i>	degrees (°)
β_{100}	<i>Full width at half maximum of the (10) peak</i>	degrees (°)

GREEK SYMBOLS (CONTINUED)

Symbol	Description	Units
χ_b	Mole fraction of aromatic bridgehead carbons	-
δ	Kinetic compensation constant	-
ε	Coal porosity at time, t	- or %
$\varepsilon_{L,gv}$	Characteristic energy of interaction of gas molecules	ergs
$\varepsilon_{L,t}$	Characteristic energy of interaction of tar molecules	ergs
$\varepsilon_{L,air}$	Characteristic energy of interaction of air molecules	ergs
$\varepsilon_{L,gt}$	Characteristic energy of interaction of gas-tar mixture	ergs
$\varepsilon_{L,v-air}$	Characteristic energy of interaction of volatile-air mixture	ergs
ε_{rad}	Effective emissivity	-
$\varepsilon_{rad,s}$	Emissivity of coal particle	-
$\varepsilon_{rad,t}$	Emissivity of TGA tube	-
ϕ_j	Fractional volatile matter content of maceral, j	-
ϕ_m	Fractional volatile matter content of residual macerals	-
γ	Gamma band	-
$\eta_{dem.}$	Effectiveness of demineralization	%
κ	Boltzmann constant	ergs.K ⁻¹
λ	Wavelength of incident X-ray	Å
μ_a	Viscosity of water vapour	Pa.s
μ_g	Viscosity of heating medium (N ₂)	Pa.s
μ_v	Viscosity of volatiles	Pa.s
μ_m	Viscosity of gas product mixture (volatiles, vapour and air)	Pa.s
π	P_i	-
θ	Peak position/XRD angle of scan	degrees (°)
θ_{002}	Peak position of d_{002} peak	degrees (°)
θ_{10}	Peak position of (10) peak	degrees (°)
θ_{11}	Peak position of (11) peak	degrees (°)
ρ_a	Density of water	kg.m ⁻³
ρ_{air}	Density of air	kg.m ⁻³
ρ_{avg}	Average particle density from mercury submersion	kg.m ⁻³

GREEK SYMBOLS (CONTINUED)

Symbol	Description	Units
$\rho_{t,Hg}$	Density of mercury	kg.m ⁻³
ρ_{coal}	Distribution of coal particle density	kg.m ⁻³
ρ_i	Density for species, <i>i</i>	kg.m ⁻³
$\rho_{i,0}$	Initial density of species, <i>i</i>	kg.m ⁻³
ρ_p	Particle density from mercury submersion	kg.m ⁻³
$\rho_{s,0}$	Initial coal particle density	kg.m ⁻³
ρ_s	Coal particle density at time, <i>t</i>	kg.m ⁻³
$\rho_{s,k}$	Skeletal density	kg.m ⁻³
ρ_g	Density of heating medium (N ₂)	kg.m ⁻³
ρ_v	Density of released volatiles	kg.m ⁻³
$\rho_{v,t}$	Density of total gas product mixture	kg.m ⁻³
σ	Standard deviation of DAEM distribution	kJ.mol ⁻¹
$\sigma+1$	Number of attachments per cluster	-
σ_{air}	Collision diameter of air	Å
σ_b	Stefan-Boltzmann constant	W.m ⁻² .K ⁻⁴
σ_{gv}	Collision diameter of gaseous volatiles	Å
σ_{gt}	Collision diameter of gas-tar mixture	Å
σ_t	Collision diameter of tar	Å
σ_v	Collision diameter of volatiles	Å
σ_{vair}	Collision diameter of volatile-air mixture	Å
τ	Tortuosity	-
ξ_a	Fractional contribution of moisture to the total volatiles	-
ξ_b	Fractional contribution of peak <i>b</i> to the total volatiles	-
ξ_g	Fractional contribution of peak <i>g</i> to the total volatiles	-
ξ_i	Fractional contribution of component <i>i</i> , to the total volatiles	-
ξ_i^*	Moisture fraction free, fractional contribution of component <i>i</i> , to the total volatiles	-
ζ_j	Percentage contribution of maceral, <i>j</i>	%
$\Omega_{D,i}$	Mass transfer collision integral for species, <i>i</i>	-

GREEK SYMBOLS (CONTINUED)

Symbol	Description	Units
$\Omega_{D,j}$	<i>Mass transfer collision integral for species, j</i>	-
$\Omega_{D,i,j}$	<i>Mass transfer collision integral for specie mixture, i-j</i>	-
$\Omega_{D,gt}$	<i>Mass transfer collision integral for tar-gas mixture</i>	-
$\Omega_{D,vair}$	<i>Mass transfer collision integral for volatile-air mixture</i>	-
Ω_v	<i>Collision integral</i>	-
$\Omega_{v,i}$	<i>Collision integral for species, i</i>	-
$\Omega_{v,g}$	<i>Collision integral for devolatilization gas</i>	-
$\Omega_{v,t}$	<i>Collision integral for tars</i>	-

ABBREVIATIONS:

ACT	:	Advanced coal technology
a.d.b	:	Air dry basis
a.f.b	:	Ash free basis
AFROX	:	African Oxygen
ALG	:	Alginite
ASTM	:	American Society for Testing Materials
BD	:	Block decay
BET	:	Brunauer-Emmett-Teller
BJH	:	Barret-Joyner-Halenda
BTX	:	Benzene, toluene and xylene
calc	:	Calculated
CCSEM	:	Computer controlled scanning electron microscopy
CM1	:	Conductivity model 1
CM2	:	Conductivity model 2
CPD	:	Chemical percolation devolatilization model
CP-MAS	:	Cross-polarization with magic-angle-spinning
CRMP	:	CO ₂ reforming methane process conditions
CSA	:	Chemical shielding anisotropy

ABBREVIATIONS (CONTINUED):

C.V.	:	Calorific value
d.a.f.	:	Dry, ash free basis
d.b	:	Dry basis
DAEM	:	Distributed activation energy model
DAN	:	Dialkyl substituted naphthalene
DSC	:	Differential Scanning Calorimetry
DD	:	Dipolar dephasing
DEPT	:	Distortionless enhancement by polarization
DOE	:	Department of Energy
D-R	:	Dubinin-Radushkevich
DTG	:	Differential thermogravimetric/thermogravimetry
DTI	:	Department of trade and industry
EIA	:	Energy Information Administration
exp	:	Experimental
FFT	:	Fast Fourier Transform
FG-DVC	:	Functional Group-Depolymerisation Vaporization Cross linking
FID	:	Flame ionization detection/detector (for GC work)
FID	:	Free induction decay (for NMR work)
FIMS	:	Field ionization mass spectrometry
F/SEC	:	Fusinite/Secretinite
FSI	:	Free swelling index
FTIR	:	Fourier transform infrared spectroscopy
FWHM	:	Full width at half maximum
G#5	:	Abbreviation used for coal obtained from Witbank seam 5
GC	:	Gas chromatography
HMB	:	Hexamethylbenzene
HPLC	:	High performance liquid chromatography
HRTEM	:	High resolution transmission electron microscopy
I INT	:	Inert Inertodetrinite
INY	:	Abbreviation used for coal obtained from Witbank seam 2
ISF	:	Inert semifusinite
ISO	:	International Standards Organization

ABBREVIATIONS (CONTINUED):

LCPs	:	Liquid crystalline polymers
LOIF	:	Loss of ignition free basis
LPTGA	:	Large Particle Thermogravimetric Analysis/Analyzer
MALDI-TOF	:	Matrix assisted laser-desorption ionization, time-of flight
MI	:	Maceral Index
MIC	:	Micrinite
MS	:	Mass spectrometry
MSCs	:	Molecular sieving carbons
MSD	:	Mass selective detector
MPRM	:	Multiple, parallel reaction model
MSRM	:	Multiple, stage reaction model
m.m.b.	:	Mineral matter basis
m.m.f.b	:	Mineral matter free basis
MUMPS	:	Multifrontal Massively Parallel Sparse
NMP	:	N-methyl-2-pyrrolidinone
NMR	:	Nuclear magnetic resonance spectroscopy
ODE	:	Ordinary differential equation
PAHs	:	Polycyclic aromatic hydrocarbons
PBN	:	Poly(butylene terephthalate)
PDE	:	Partial differential equation
PEN	:	Poly(ethylene naphthalate)
PONA	:	Paraffins, olefins, naphthenes and aromatics
Prox	:	Proximate
PTFE	:	Polytetrafluorethylene
PV	:	Pseudo-vitrinite
Py-GC-MS	:	Pyrolysis- gas chromatography-mass spectrometry
Py-MS	:	Pyrolysis- mass spectrometry
R&D	:	Research and Development
RID	:	Refractive index detection/detector
R INT	:	Reactive Inertodetrinite
ROM	:	Run of mine
RSF	:	Reactive semifusinite

ABBREVIATIONS (CONTINUED):

SABS	:	South African Bureau of Standards
SANS	:	South African National Standard
SEC	:	Size exclusion chromatography
S.e.c.s.	:	Sequential elution solvent chromatography
SIMDIST	:	Simulated distillation
SPE	:	Single pulse excitation
S/R/C	:	Sporinite/Resinite/Cutinite
SRM	:	Single reaction model
SSB	:	Spinning sideband
<i>sym</i> -OHAn	:	<i>sym</i> -octahydroanthracene
<i>sym</i> -OHP	:	<i>sym</i> -octahydrophenanthrene
TBE	:	Tetrabromo-ethane
TCD	:	Thermal conductivity detection/detector
TCR	:	Tar capturing reactor
TG	:	Thermogravimetric/thermogravimetry
TGA	:	Thermogravimetric Analyzer
THF	:	Tetrahydrofuran
TI	:	Total inertinite
TIC	:	Total ion chromatogram
TKS	:	Tetrakis(trimethylsilyl)silane
TL	:	Total liptinite
TMS	:	Tetramethylsilane
TSH	:	Abbreviation used for coal obtained from the Venda-Pafuri district
TV	:	Total vitrinite
UHP	:	Ultra high purity
Ult	:	Ultimate
UMZ	:	Abbreviation used for coal obtained from Witbank seam 4
USB	:	Universal serial bus
UV	:	Ultra violet
VIS	:	Visible light detector
VIT	:	Vitrinite
vol.%	:	Volume percentage

ABBREVIATIONS (CONTINUED):

WCI	:	World Coal Institute
wt. %	:	Weight percentage
XRD	:	X-Ray Diffraction
XRF	:	X-Ray Fluorescence
XPS	:	X-ray photoelectron spectroscopy

Glossary

“Advanced analyses” refers to more advanced analytical strategies applied for assessing the molecular properties of coal and coal-derived products and includes analyses such as: GC-FID, GC-MS, NMR, HRTEM, XRD, MALDI-TOF MS, SEC, etc.

“Conventional analyses” refers to standard analytical techniques applied in the coal research domain and includes methods such as: proximate-, ultimate-, calorific value-, petrographic-, mercury porosimetry analyses, etc.

“Core temperature” refers to the temperature measured at the centre of the coal particle.

“Devolatilization” refers to the process of tar, water and gas evolution, including char production, via the thermal degradation of coal under an inert atmosphere. This process is also more commonly referred to as pyrolysis.

“G#5” refers to the abbreviation used for the vitrinite-rich coal sample obtained from seam 5 of the Witbank coalfields.

“INY” refers to the abbreviation used for the inertinite-rich coal sample obtained from seam 2 of the Witbank coalfields.

“Loss free basis” refers to the normalisation of product yields by taking into account any loss in product material that could have occurred during product separation, removal and/or measurement.

“Molecular properties” refers to characteristic properties describing the molecular structure of coal and includes properties such as aromaticity, molecular mass distribution, fraction of amorphous carbon.

“Non-fuel use of coal” refers to the exclusive usage of coal for other applications than electricity generation and the production of fuels. This includes application of coal for the production of aromatic chemicals and/or higher value carbons such as graphites.

“Pseudo-component” refers to a group of chemical entities displaying similar reaction behaviour and can be described by a lumped average of kinetic parameters.

“Pseudo-isothermal conditions” refers to devolatilization of coal particles under isothermal reactor conditions i.e.: introduction of coal particles into the reactor or TG which is controlled at an isothermal set point.

“Thermophysical properties” refers to coal specific properties related to heat transfer parameters such as the thermal conduction and heat capacity of a coal.

“Thermoplasticity or thermoplastic nature” refers to the swelling and/or -shrinkage behaviour of coal.

“TSH” refers to the abbreviation used for the vitrinite-rich coal sample obtained from seam 1 and 2 of the Venda-Pafuri coalfields.

“UMZ” refers to the abbreviation used for the inertinite-rich coal sample obtained from seam 4 of the Witbank coalfields.